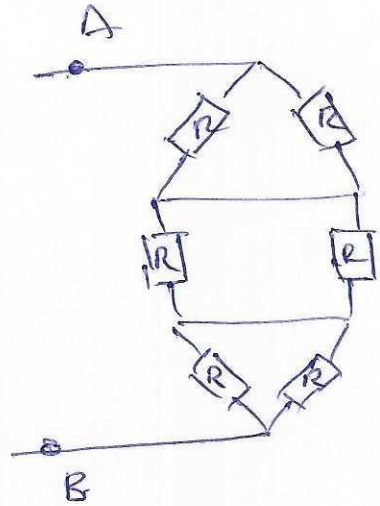


Exo 1 : Calcul de R_{AB}

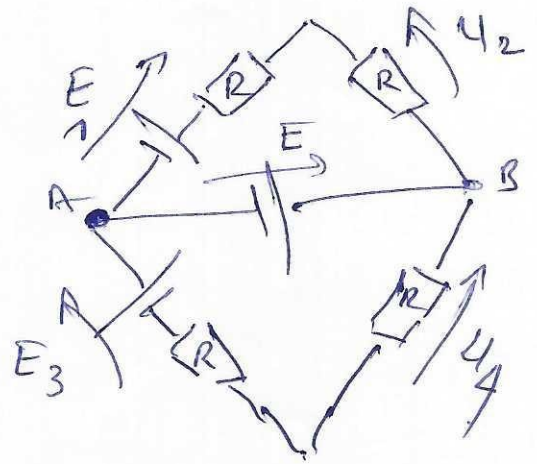
$$R_{AB} = \frac{3}{2} R$$



Exo 2 :

$$U_2 = \frac{E_1 - E}{2}$$

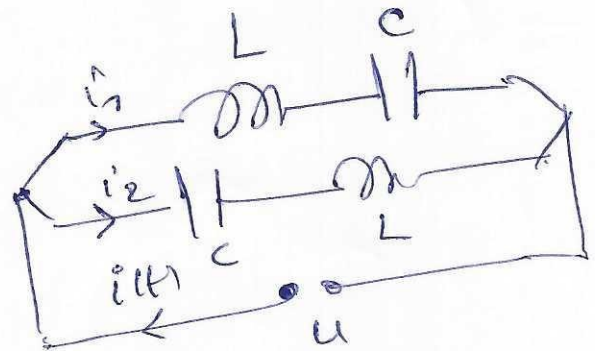
$$U_4 = \frac{E + E_3}{2}$$



Exo 3

$$u(t) = U_m \sin \omega t$$

$$i(t) = I_m \sin(\omega t + \varphi)$$



1/ $Z_{ep} = ?$

$$Z_{ep} = j \frac{1}{2} \left(L\omega - \frac{1}{C\omega} \right)$$

$$\Rightarrow \begin{cases} X(\omega) = 0 \\ Y(\omega) = \frac{1}{2} \left(L\omega - \frac{1}{C\omega} \right) \end{cases}$$

2/ Déphasage φ

$$\bar{U} = Z_{ep} \bar{I}$$

$$\Rightarrow \arg \bar{U} = \arg Z_{ep} + \arg \bar{I}$$

$$\varphi = -\arg Z_{ep}$$

$$\Rightarrow \varphi = -\frac{\pi}{2}$$

$$3- \quad \omega_0 = ?$$

$$\operatorname{Im}(Z_{eq}) = 0$$

$$L\omega_0 - \frac{1}{C\omega_0} = 0 \Rightarrow$$

$$\boxed{\omega_0 = \frac{1}{\sqrt{LC}}}$$

4-

$$U = Z_{eq} i$$

$$U_m e^{j\omega t} = Z_{eq} I_m e^{j(\omega t + \varphi)}$$

$$\boxed{I_m = \frac{U_m}{\|Z_{eq}\|} = \frac{U_m}{L\omega - \frac{1}{C\omega}}}$$

5-

$$i_1 = i_2$$

Parce que les 2 branches contiennent les mêmes composants

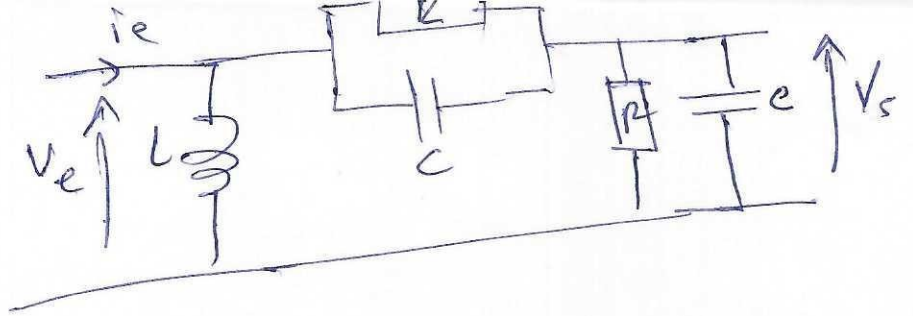
6-

D'après la loi des noeuds

$$i_1 + i_2 = i \quad \text{avec} \quad i_1 = i_2$$

$$\Rightarrow \text{ou} \quad \boxed{i_1 = i_2 = \frac{i}{2}}$$

3/ Exo 4:



1 - $H(j\omega) = \frac{1}{2}$

2 - On suppose que $H(j\omega) = \frac{K}{1 + j\frac{\omega}{\omega_c}}$

$$G(\omega) = \frac{K}{\sqrt{1 + \left(\frac{\omega}{\omega_c}\right)^2}}$$

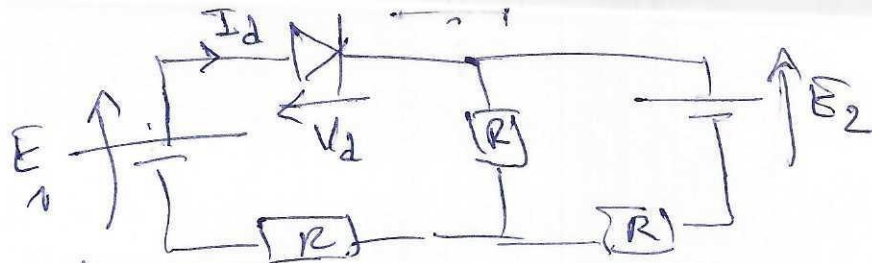
$$G_{dB} = \lg k - 10 \lg \left(1 + \left(\frac{\omega}{\omega_c}\right)^2\right)$$

4 - $\phi(\omega) = ?$

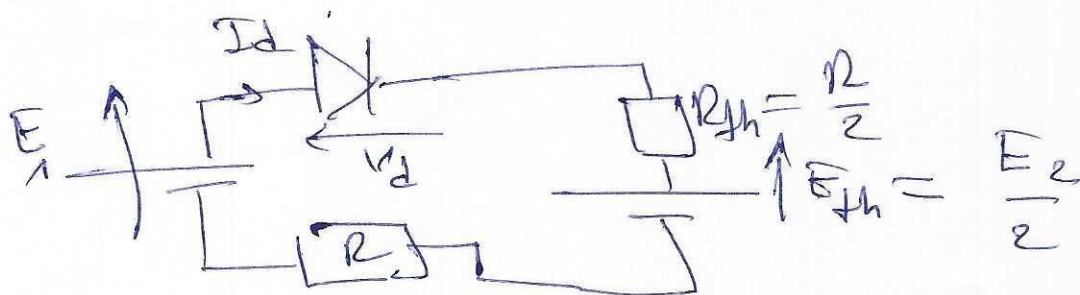
$$\phi(\omega) = \arg H(j\omega) = -\arctan \frac{\omega}{\omega_c}$$

$$\boxed{\phi(\omega) = -\arctan \frac{\omega}{\omega_c}}$$

4/ Exo 5



1- Appliquant le Th de Thevenin.



La loi des mailles : $E_1 - V_d - \frac{R}{2} I_d - \frac{E_2}{2} - \frac{R}{2} I_d = 0$

$$E_1 - \frac{E_2}{2} - V_d - \frac{3R}{2} I_d = 0$$

d'où
$$I_d = \frac{2E_1 - E_2}{3R} - \frac{2V_d}{3R}$$

2- Deux points particuliers.

Pour $I_d = 0$

$$V_d = \frac{2E_1 - E_2}{2}$$

Pour $V_d = 0$

$$I_d = \frac{2E_1 - E_2}{3R}$$

d'où
$$A \left(0, \frac{2E_1 - E_2}{2} \right)$$

$$B \left(\frac{2E_1 - E_2}{3R}, 0 \right)$$

3 - Modèle avec Seuil. $V_d = V_0$

a - Diode Bloquée

$$I = \frac{E_2}{2R}$$

b - Diode passante

On a $I = I_1 + I_2$

Maille ① $E_1 - V_0 - RI - RI_1 = 0$

d'où $I_1 = \frac{E_1 - V_0}{R} - I$ (*)

Maille ② $E_2 - RI - RI_2 = 0$

d'où $I_2 = \frac{E_2}{R} - I$ (**)

(*) et (**) On a :

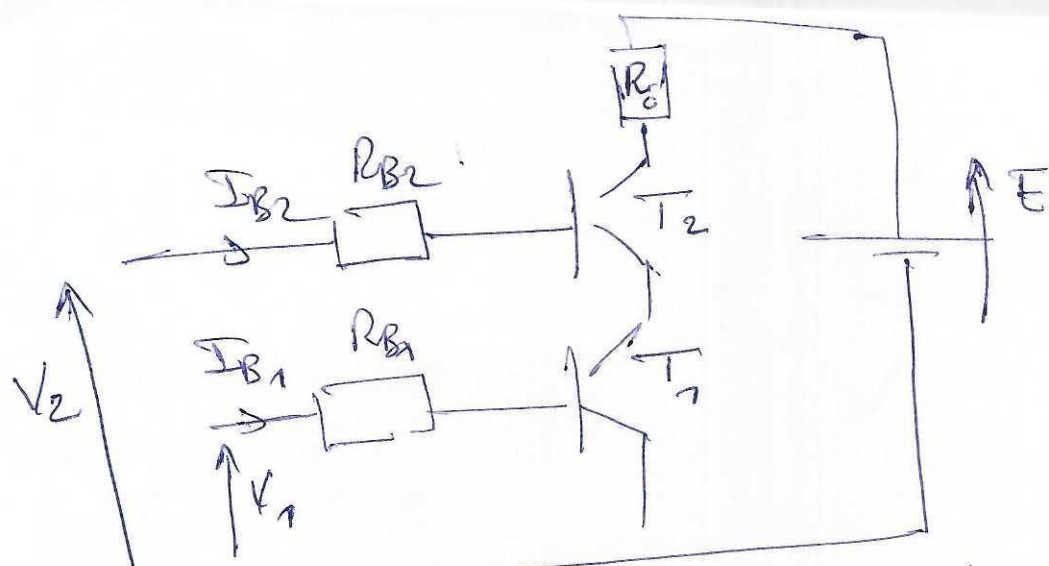
$$I = \frac{E_1 - V_0}{R} - I + \frac{E_2}{R} - I$$

$$3I = \frac{E_1 - V_0 + E_2}{R}$$

d'où

$$I = \frac{E_1 + E_2 - V_0}{3R}$$

Exo 6



T_1 et T_2 identiques et fonctionnent en mode normal.

1- T_1 et T_2 : NPN

2- I_{B1} et I_{C1} : la loi des mailles :

$$V_1 - R_{B1} I_{B1} - V_{BE} = 0$$

$$I_{B1} = \frac{V_1 - V_{BE}}{R_{B1}} \quad \text{A.N.} \quad I_{B1} = 34 \mu A$$

$$I_{C1} = \beta I_{B1} \quad \text{A.N.} \quad I_{C1} = 68 \text{ mA}$$

• I_{C2} , I_{B2} : On a $I_{C1} = I_{C2} = (\beta + 1) I_{B2}$

$$\text{donc} \quad I_{B2} = \frac{I_{C1}}{\beta + 1} \quad \text{A.N.} \quad I_{B2} =$$

$$I_{C2} = \beta I_{B2} \quad \text{A.N.} \quad I_{C2} =$$